

# Time-delay Tolerant Control of an Omnidirectional Multi-agent System for Transport Operations

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October 12, 2018

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# Introduction

## Multi-Agent Systems

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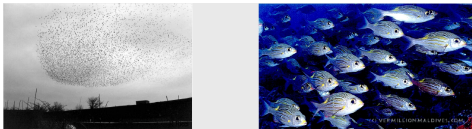
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- The problem of synchronization of multiple agents arises in numerous applications, both in natural and in man-made systems.
- Examples from nature include:



Bird flock, fish school and collective transport

# Introduction

## Context and Main Goal



### Introduction

Motivation

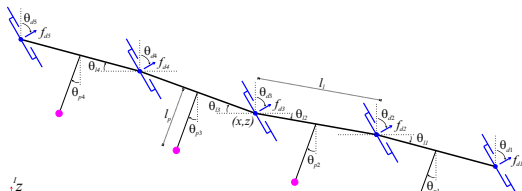
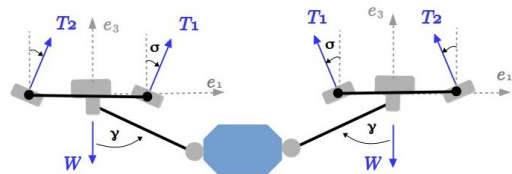
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# Introduction

## Aerogripper concept

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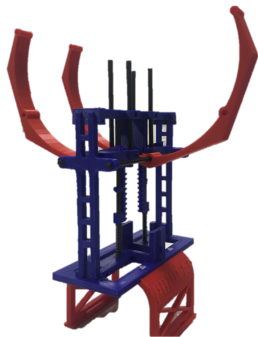
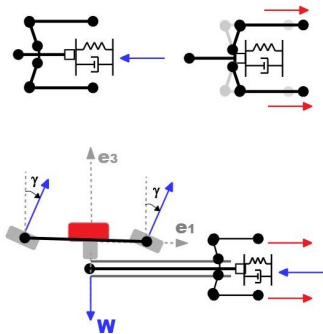
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# Introduction

## Optimal Grasping Points Identification

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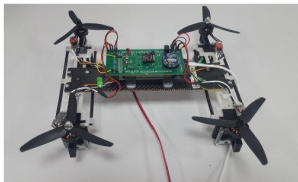
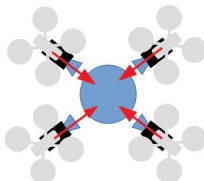
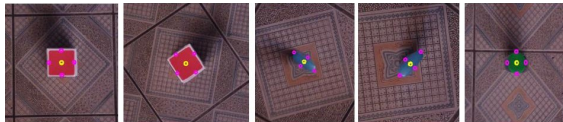
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During grasping or manipulation operations, contacts between the end-effectors and the object depend on different aspects, such as: friction, vector force direction and magnitude. A reliable contact point between the gripper and the object is considered as optimal if the grabbing force is orthogonal to the object's surface.



# System Modeling

## Single Agent Modeling

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- Time-delay Control of an Omnidirectional Multi-agent System for Transport Operations.  
J. U. Alvarez-Muñoz, J. Escareno, F. Méndez-Barrios, I. Boussaada and S. I. Niculescu  
22nd IEEE International Conference on System Theory, Control and Computing, Sinaia, Rumania (presented yesterday!)
- Time-delay-based PID Control of an Omnidirectional Multi-agent System for Transport Operations  
J. U. Alvarez-Muñoz, J. Escareno, F. Méndez-Barrios, I. Boussaada and S. I. Niculescu  
Submitted to 2019 AMERICAN CONTROL CONFERENCE, PHILADELPHIA, USA

A single agent is represented by an holonomic mobile robot evolving within the 2D space, featuring actuated translational and rotational motion.

### The translational and rotational dynamics

$$\Sigma_{tra}^I : \begin{cases} \dot{\xi} = \mathbf{v} \\ M\dot{\mathbf{v}} + mge_z = Rf^B \end{cases} \quad (1)$$

$$\Sigma_{rot}^B : \begin{cases} \dot{R} = R\Omega^\times \\ I\dot{\Omega} + I\Omega \times \Omega = \Gamma \end{cases} \quad (2)$$

# System Modeling

## Single Agent Modeling

The torques  $\tau$  and forces  $f$ , in the body frame  $B$ , are given as follows

$$\begin{aligned} \mathbf{f}^B &= (f_u, f_v, f_w)^T \\ \boldsymbol{\tau}^B &= (\tau_p, \tau_q, \tau_r)^T \end{aligned} \quad (3)$$

Considering that the agents are fully actuated, the dynamic equations are

$$M(\mathbf{q})\ddot{\mathbf{q}} + C(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{G}(\mathbf{q}) = \mathbf{U}, \quad (4)$$

$$M(\mathbf{q}) = \begin{bmatrix} \mathbb{M} & \mathbf{0} \\ \mathbf{0} & \mathbb{I}\mathcal{W}_n \end{bmatrix}; C(\mathbf{q}, \dot{\mathbf{q}}) = \begin{bmatrix} \mathbb{M} & \mathbf{0} \\ \mathbf{0} & \dot{\mathcal{W}}_n \dot{\boldsymbol{\eta}} + \mathbb{I}(\mathcal{W}_n \boldsymbol{\eta}) \times (\mathcal{W}_n \boldsymbol{\eta}) \end{bmatrix} \quad (5)$$

$$\mathbf{G}(\mathbf{q}) = \begin{bmatrix} m\mathbf{g}e_z \\ \mathbf{0} \end{bmatrix}; \mathbf{U} = \begin{bmatrix} R\mathbf{f}^B \\ \boldsymbol{\tau} \end{bmatrix} \quad (6)$$

and considering the vectors

$$\mathbf{q} = (\boldsymbol{\xi}, \boldsymbol{\eta})^T \in \mathbb{R}^6 \quad (7)$$

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# System Modeling

## Multi-agent Dynamics

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We restrict the motion profile of the  $i^{\text{th}}$  agent to the horizontal plane ( $e_x - e_y$  plane). This renders Eq.(4) into

$$\ddot{\mathbf{q}}_{(i)} = M(\mathbf{q})^{-1}(\mathbf{U}) \quad (8)$$

where

$$M(\mathbf{q})_{(i)} = \begin{bmatrix} M_{2 \times 2} & 0 \\ 0 & I_y \end{bmatrix}; \mathbf{U}_{(i)} = \begin{bmatrix} R\mathbf{f}^B \tau_\psi \end{bmatrix} \quad (9)$$

The corresponding adjacency matrix is

$$\mathcal{A} = [a_{ij}] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix} \quad (10)$$

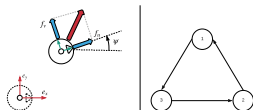


Figure: [left] Single agent freebody sketch, [right] Cyclic topology

# Control Strategy

## Consensus and Time Delay Control Law

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It is possible to find an input-state linearization

$$\ddot{\mathbf{q}}_{(i)} = \boldsymbol{\nu} \quad (11)$$

whose control input can be split as

$$\ddot{\mathbf{q}}_{(i)} = \boldsymbol{\nu}_{int(i)} + \boldsymbol{\nu}_{c(i)} \quad (12)$$

The position/trajectory of the geometrical flock's center of mass. Hence, Eq.(13) is

$$\begin{aligned} \ddot{\mathbf{q}}_{(i)} = & -\sum_{j=1}^m \alpha_{ij}(\mathbf{q}_{(i)} - \mathbf{q}_{(j)}) \\ & -\sum_{j=1}^m \beta_{ij}(\dot{\mathbf{q}}_{(i)} - \dot{\mathbf{q}}_{(j)}) + \ddot{\mathbf{q}}_{(j)} + \boldsymbol{\nu}_{c(i)} \end{aligned} \quad (13)$$

The model for the multi-agent system considering the time delay

$$\begin{aligned} \ddot{\mathbf{q}}_{(i)}(t) = & -\sum_{j=1}^m \alpha_{ij}(\mathbf{q}_{(i)}(t - \tau_{1ij}) - \mathbf{q}_{(j)}(t - \tau_{1ij})) \\ & -\sum_{j=1}^m \beta_{ij}(\dot{\mathbf{q}}_{(i)}(t - \tau_{1ij}) - \dot{\mathbf{q}}_{(j)}(t - \tau_{1ij})) \\ & + \ddot{\mathbf{q}}_{(j)}(t) + \boldsymbol{\nu}_{c(i)} \end{aligned} \quad (14)$$

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## Consensus and Time Delay Control Law

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After denoting the consensus protocol in terms of error and taking the Laplace transform, one obtains

$$s^2 E(s) + \sum \alpha e^{-\tau_{1ij} s} E(s) + \sum \beta s e^{-\tau_{1ij} s} E(s) = 0 \quad (15)$$

Then, the corresponding quasipolynomial function is given by

$$\Delta(s, \tau) = s^2 + \alpha e^{-s\tau} + \beta s e^{-s\tau} \quad (16)$$

where  $\beta \neq 0$ .

For any  $\tau \in \mathbb{R}_+$  there exist a stabilizing pair  $(\alpha, \beta) \in \mathbb{R}_+^2$ .

$$\alpha(\sigma) = (2 - \tau\sigma) \sigma e^{-\sigma\tau}, \quad (17)$$

$$\beta(\sigma) = (1 - \tau\sigma) \sigma^2 e^{-\sigma\tau}. \quad (18)$$

Then,  $\Delta$  is asymptotically stable whenever  $0 < \sigma < \frac{1}{\tau}$ . If in addition  $\sigma = \frac{2-\sqrt{2}}{\tau}$ , then such a solution is dominant.

# Control Strategy

## Multi-agent Formation Control

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Each agent consists of an attitude and position controllers. Now, considering the state  $q = (\xi, \dot{\xi}, \eta_x, \dot{\eta}_x, \eta_y, \dot{\eta}_y)$  for every agent, the average attitudes and linear positions are

$$\xi_C = \frac{1}{N} \sum_{i=1}^N \xi_i \quad \dot{\xi}_C = \frac{1}{N} \sum_{i=1}^N \dot{\xi}_i \quad (19)$$

$$\eta_{CM_x} = \frac{1}{N} \sum_{i=1}^N \eta_{i_x} \quad \dot{\eta}_{CM_x} = \frac{1}{N} \sum_{i=1}^N \dot{\eta}_{i_x} \quad (20)$$

$$\eta_{CM_y} = \frac{1}{N} \sum_{i=1}^N \eta_{i_y} \quad \dot{\eta}_{CM_y} = \frac{1}{N} \sum_{i=1}^N \dot{\eta}_{i_y} \quad (21)$$

Assuming that the agent 1 is the leader, a consensus algorithm to reach an agreement for orientation and position can be given by

$$u_{1\xi} = -\lambda_1 \text{sat}(\xi_C^d - \xi_C) - \lambda_2 \text{sat}(\dot{\xi}_C^d - \dot{\xi}_C) \quad (22)$$

$$u_{1x} = -\lambda_3 \text{sat}(\eta_{CM_x}^d - \eta_{CM_x}) - \lambda_4 \text{sat}(\dot{\eta}_{CM_x}^d - \dot{\eta}_{CM_x}) \quad (23)$$

$$u_{1y} = -\lambda_5 \text{sat}(\eta_{CM_y}^d - \eta_{CM_y}) - \lambda_6 \text{sat}(\dot{\eta}_{CM_y}^d - \dot{\eta}_{CM_y}) \quad (24)$$

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Let  $\Delta$  be a set of relative, desired inter-agent distances, that is

$$\Delta = [\delta_{ij} \in \mathbb{R} | \delta_{ij} > 0; \quad i, j = 1, \dots, N, i \neq j] \quad (25)$$

It is possible to extend the consensus algorithms to formation control if the formation is represented by vectors of relative attitudes or linear positions of neighboring agents.

$$\ddot{\mathbf{q}}_{(i)} = -\sum a_{ij} K(\mathbf{q}_{(i)} - \mathbf{q}_{(j)} - \delta_{ij}) - \sum a_{ij} K(\dot{\mathbf{q}}_{(i)} - \dot{\mathbf{q}}_{(j)} + \ddot{\mathbf{q}}_{(j)} + \nu_{c(i)}) \quad (26)$$

with  $K \in \mathbb{R} > 0$

# Simulation Results

## Simulation Scenario

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The simulation consists on three stages.

- The robot multi-agent system is initialized at the states given by the Table 1. Then, it is sent to  $p_o = [1 \ 1]^T m$ . Orientation consensus is performed to  $\xi_i^d = (-90^\circ - 210^\circ 30^\circ)$ . The contact points are located at  $\eta_1^d = [0.95 \ 0.99]^T m$ ,  $\eta_2^d = [1 \ 1.085]^T m$  and  $\eta_3^d = [1.05 \ 0.99]^T m$ .
- A trajectory tracking consensus is performed between the time 15s and 60s and it is given by  $\eta_{CM_x}^d = 0.5 \sin(0.07t + 1.5)$  and  $\eta_{CM_y}^d = 0.25 \sin(0.1t + 1.27)$ .
- When the object center of mass reaches the desired place, given by  $p_{od} = [2 \ 1.5]^T m$ , the multi-agent system drops the object.

Table: Initial conditions

Robot	Orientation ( $\xi_i$ )	Position $\eta_{ix}$	Position $\eta_{iy}$
1	15°	0.85m	-0.6m
2	5°	0.1m	0.25m
3	-10°	-0.6m	1.05m

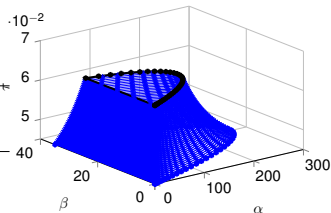


Figure: 3D– Region in the  $\alpha - \beta$  parameter space, for  $\tau \in [0.045, 0.065]$ .

# Simulation Results

## Simulation Scenario

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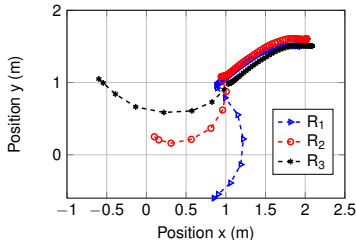
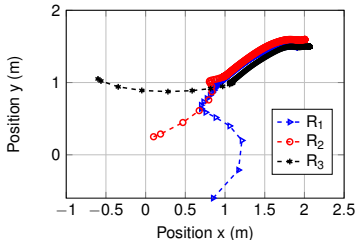
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**Figure:** 2d positions of the three agents during the simulation. (Top) without communication delay, (bottom) with communication delay

# Simulation Results

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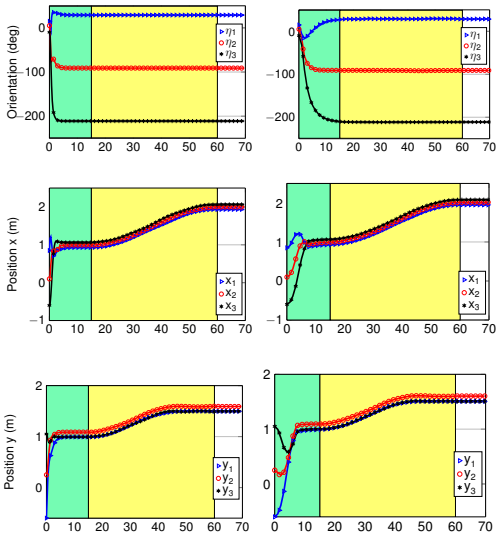
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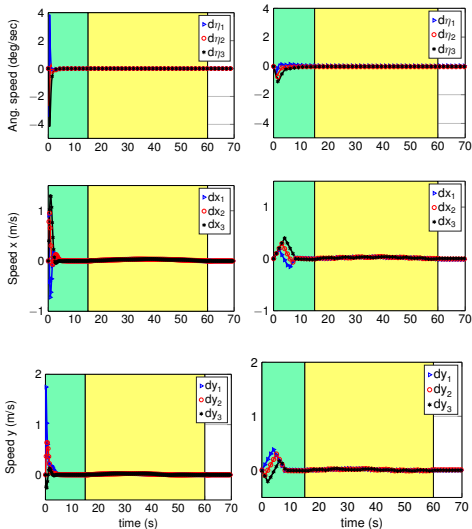
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### Conclusions

- A control methodology is described to stabilize the collective motion (consensus) regarding the transport operations.
- Such a control strategy consists on a time-delay tolerant control law, which guarantees the stabilization of an individual agent.
- Explicit stability regions for a range of delays concerning the proposed quasipolynomial is presented and explained.
- Simulation results show the effectiveness of the proposed multi-agent control methodology for an object transport scenario.
- The simulation allows also to perform a comparison between a time-delay multi-agent system and simple multi-agent system.

### Perspectives

- Explicit presentation and explanation of the object contact points and coordinated object avoidance will be discussed.

Thank You

