



# Motor and Perception Constrained NMPC for Torque-controlled Generic Aerial Vehicles

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## Objectives

Introduction

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- ▶ Extend previous work with a more complete version [1]
- Define a NMPC framework for generic UAVs
- Use motor-torque level controls
- Include actuation and perception constraints

<sup>[1]</sup> Jacquet *et al.*, "Perception-constrained and Motor-level Nonlinear MPC for both Underactuated and Tilted-propeller UAVs."







#### Motivations

- Handle motion tasks with critical perception objectives
- Maintain visibility over a set of markers for localization
- Track a mobile phenomenon with maximum time coverage
- Maintain safety distance with the environment





# Part I: System modeling



## Generically Tilted Multi Rotor









#### System state

$$\mathbf{x}_{body} = [\mathbf{p}^{\top} \mathbf{q}^{\top} \mathbf{v}^{\top} \boldsymbol{\omega}^{\top}]^{\top} \in \mathbb{R}^{3} \times \mathbb{S}^{3} \times \mathbb{R}^{3} \times \mathbb{R}^{3},$$
(1a)  
$$\mathbf{x}_{actuators} = \gamma, \text{ with } \gamma = [f_{1}...f_{n}]^{\top},$$
(1b)

### System input

$$\dot{\gamma} = \mathbf{u},$$
 (2)

The forces  $\gamma$  and their derivatives  $\dot{\gamma}$  are linked to the rotors' speeds and accelerations doing a change of coordinates [2]



<sup>[2]</sup> Bicego *et al.*, "Nonlinear model predictive control with enhanced actuator model for multi-rotor aerial vehicles with generic designs."



#### Kinematic and Dynamic equations

$$\dot{\mathbf{p}} = \mathbf{v}$$
 (3a)

$$\dot{\mathbf{q}} = \frac{1}{2} \begin{bmatrix} 0\\ \omega \end{bmatrix} \otimes \mathbf{q}$$
 (3b)

$$\begin{bmatrix} \dot{\mathbf{v}} \\ \dot{\boldsymbol{\omega}} \end{bmatrix} = \begin{bmatrix} m\mathbf{I}_3 & \mathbf{O}_3 \\ \mathbf{O}_3 & \mathbf{J} \end{bmatrix}^{-1} \left( \begin{bmatrix} -mg\mathbf{z}_W \\ -\boldsymbol{\omega} \times \mathbf{J}\boldsymbol{\omega} \end{bmatrix} + \begin{bmatrix} \mathbf{q} \otimes \mathbf{G}_f \gamma \otimes \mathbf{q}^* \\ \mathbf{G}_\tau \gamma \end{bmatrix} \right)$$
(3c)

with  $\mathbf{G}_f$  and  $\mathbf{G}_{\tau} \in \mathbb{R}^{3 \times n}$  respectively being the *force* and *torque allocation matrices* [3]

<sup>[3]</sup> Michieletto *et al.*, "Fundamental Actuation Properties of Multirotors: Force-Moment Decoupling and Fail-Safe Robustness."





#### **Realistic actuation constraints**

$$\underline{\gamma} \leq \mathbf{x}_{s} \leq \overline{\gamma}$$
 (4a)  
 $\underline{\dot{\gamma}}(\gamma) \leq \mathbf{u} \leq \overline{\dot{\gamma}}(\gamma)$  (4b)

## Where $\dot{\gamma}(\gamma)$ and $\overline{\dot{\gamma}}(\gamma)$ are known through an identification campaign [2]

**CNIS** System modeling / Constraints



<sup>[2]</sup> Bicego *et al.*, "Nonlinear model predictive control with enhanced actuator model for multi-rotor aerial vehicles with generic designs."





Decoupled vertical and horizontal FOV constraints:

$$|x_M/z_M| \leq anrac{lpha_h}{2}, \quad |y_M/z_M| \leq anrac{lpha_v}{2}.$$





(5)



#### Feature tracking objective



Minimization of the angular distance between the feature and the sensor principal axis [4]

[4] Penin *et al.*, "Vision-Based Reactive Planning for Aggressive Target Tracking While Avoiding Collisions and Occlusions."

CNIS System modeling / Constraints





#### Optimal control problem

$$\min_{\substack{\mathbf{x}_{0},\ldots\mathbf{x}_{N}\\\mathbf{u}_{0},\ldots\mathbf{u}_{N-1}}} \sum_{k=0}^{N} \|\mathbf{y}_{k} - \mathbf{y}_{r,k}\|_{\mathbf{Q}}^{2} \tag{6a}$$

$$\mathbf{s.t.} \quad \mathbf{x}_{0} = \mathbf{x}(t) \tag{6b}$$

$$\mathbf{x}_{k+1} = \mathbf{f}(\mathbf{x}_{k}, \mathbf{u}_{k}), \qquad k \in \{0, N-1\} \tag{6c}$$

$$\mathbf{y}_{k} = \mathbf{h}(\mathbf{x}_{k}, \mathbf{u}_{k}, \mathbf{p}_{M_{k}}), \qquad k \in \{0, N\} \tag{6d}$$

$$\frac{\gamma}{2} \leq \gamma_{k} \leq \overline{\gamma}, \qquad k \in \{0, N\} \tag{6d}$$

$$\frac{\dot{\gamma}_{k}}{k} \leq \mathbf{u}_{k} \leq \overline{\dot{\gamma}}_{k}, \qquad k \in \{0, N-1\} \tag{6f}$$

$$|\mathbf{x}_{M}/\mathbf{z}_{M}|_{k} \leq \tan \alpha_{h}, \qquad k \in \{0, N\} \tag{6g}$$

$$|\mathbf{y}_{M}/\mathbf{z}_{M}|_{k} \leq \tan \alpha_{v}, \qquad k \in \{0, N\} \tag{6h}$$

with the objective vector  $\mathbf{y} = [\mathbf{p}^\top \ \mathbf{q}^\top \ \dot{\mathbf{p}}^\top \ \boldsymbol{\omega}^\top \ \cos\beta \ \dot{\cos\beta}]^\top$ 

**CNTS** System modeling / Optimal control problem





Compute the feature position covariance  $\Sigma_M$  from the pixel covariance  $\Sigma_c = \sigma^2 I_8, \sigma \in \mathbb{R}^+$  of the 4 corners, using a 1<sup>st</sup> order approximation scheme [5]

$$\boldsymbol{\Sigma}_{M} = \sigma^{2} (\mathbf{J}_{M}^{\top} \mathbf{J}_{M})^{-1}$$
(7)

 $\mathbf{J}_M \in \mathbb{R}^{8 \times 6}$  is computed for each corner using the chain rule

[5] Fourmy *et al.*, "Absolute humanoid localization and mapping based on IMU Lie group and fiducial markers."



Part II: Results



## Software diagram



Open-source implementation available online: https://redmine.laas.fr/projects/perceptive-torque-nmpc





# Hardware platform







CNIS Results / Experimental setup



#### See video

**CNTS** Results / Experimental results





#### Achievements

- Onboard NMPC implementation for several types of UAVs
- Actuation and perception realistic limitations
- Open source implementation
- Extended non-linear model using quaternions
- Uncertainty estimation of the feature 3D-pose from the camera measurements

#### Future works

Conclusion

- Extension to multi-robot systems
- NMPC failure handling, e.g. when constraints are not feasible
- Visual-Inertial state estimation
- Replace fiducial markers with object detection algorithms







Acknowledgement















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