THE NAVIGATION AND CONTROL TECHNOLOGY INSIDE THE AR.DRONE MICRO UAV

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**Parrot

***SYSNAV

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P.-J. BRISTEAU

Collaboration

Mass-market : robustness and high stability
 Mass-market : low-cost and user-friendly





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INTRODUCTION



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OUTLINE

1 AR.DRONE HARDWARE

NAVIGATION ALGORITHMS

- Calibration
- Attitude estimation
- Velocity estimation
- Navigation scheme

3 CONTROL ARCHITECTURE

- Remote controller
- Attitude control
- Hovering control
- Pilot control

4 CONCLUSIONS



OUTLINE

AR.DRONE HARDWARE Calibration Attitude estimation Velocity estimation Navigation scheme Remote controller Attitude control Hovering control



- carbon fiber frame, highly resistant plastic structure
- four brushless motors with microcontroller and cutout system, 3500 rpm
- one battery LiPo 11.1 V, 1000 mAh, 80g
- two electronic boards
- two different hulls (expanded polypropylene)





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- Parrot P6 processor, 468 MHz
- WiFi chip (ad hoc network)
- vertical camera, 60 fps
- Linux based real-time operating system, control thread at 200 Hz





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AR.DRONE HARDWARE

NAVIGATION BOARD

INERTIAL MEASUREMENT UNIT

- 3-axis accelerometer, Bosch BMA150, FS ± 2g
- 2-axis gyrometer, invensense IDG500, FS ± 500°/s
- 1-axis gyrometer, Epson XV3700, FS ± 1500%
- Data acquisition at 200 Hz.
- $\bullet \approx 10 \text{ USD}$

• 2 Prowave ultrasonic sensors, FS 6m, 25 Hz





INERTIAL MEASUREMENT UNIT

- \bullet 3-axis accelerometer, Bosch BMA150, FS \pm 2g
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 Accelerometer calibration : least-squares optimization for misalignments, scale factors, offsets

$$Y_m = AY_r + B$$

 Gyrometer calibration : least-squares optimization for misalignments, scale factors, offsets



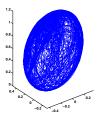
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THE NAVIGATION AND CONTROL TECH. IN THE AR.DRONE GT-UAV

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$$d_{1}$$

 d_{2}
 d_{3}
 d_{4}
 d_{4

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GT-UAV

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 Chain rule on previously calibrated accelerometers



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ONBOARD ALIGNMENT

IMU calibrated at factory but not precisely aligned with the aerial platform

- Determination of micro-rotation such that mean specific acceleration is zero during hovering
- Only roll and pitch corrections
- Execution after each take-off due to possible displacement during landing shock



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ATTITUDE ESTIMATION

Accelerometer noisy but considered debiased

$$Y_V = F - R\vec{g} + \mu_V$$

• Gyrometer noisy and biased

Observer based on complementary filter
 Orientation given by low-pass filter on accelerometer
 Angular rates given by high-pass filter on gyrometer



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IMAGES CORRECTION

• Objective of video processing : horizontal velocity

- Image compensation for angular rates
- Micro-rotations matrix from the debiased gyrometers



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$$\delta R = \begin{bmatrix} 1 & r\delta t & -q\delta t \\ -r\delta t & 1 & p\delta t \\ q\delta t & -p\delta t & 1 \end{bmatrix}$$



Two complementary algorithms

- Compensation of vertical dynamics thanks to altitude observer from ultrasonic sensors
- Optical flow technique
 - High speed
 Very low contrast sceness
- Corner tracking
 - Low speed
 Ground highly textured
- Automatic switch based on speed value and trackers number.



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- Transposition of large-size rotors modeling techniques
- Consideration of the velocities and the angular rates of the vehicle

- Blade element theory
- Consideration of the rotor in the moving body frame

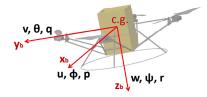


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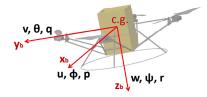
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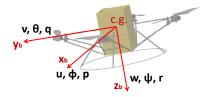
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- $\mathbf{DF}_0 = \frac{1}{2}\rho cR^2 C_{D0}\left(|\omega|(\bar{u}\mathbf{x}_b + \bar{v}\mathbf{y}_b) sgn(\omega)\bar{w}(\rho\mathbf{x}_b + q\mathbf{y}_b)\right)$
- Linear and stabilizing aerodynamic effect
- Introduction of blades flexibility

• Modifications of the lift effects mainly



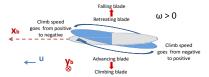
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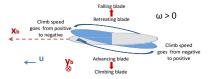
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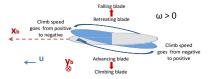


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$$\mathbf{LF} = \rho c R^3 \omega^2 C_{L\alpha} \left(\frac{\alpha_t}{3} - \frac{L}{2R|\omega|} (\varepsilon_1 q - \varepsilon_2 p) \right) \begin{bmatrix} -a \\ -b \\ 1 \end{bmatrix}$$



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AERODYNAMICS MODEL EXPLOITATION

- Existence of a linear term in the drag force induced by the rotors
- Reinforcement of this term by the blades flexibility
- Observer based on complementary filter



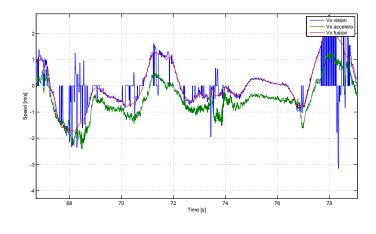
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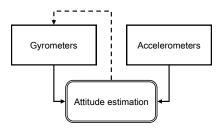


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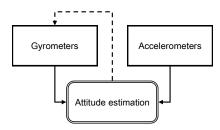


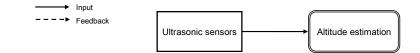




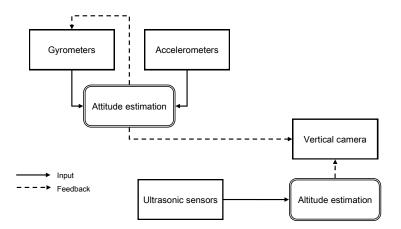




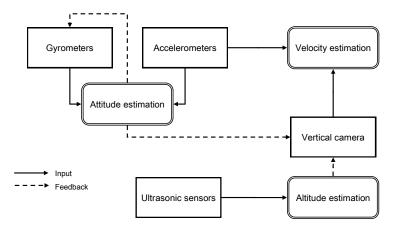




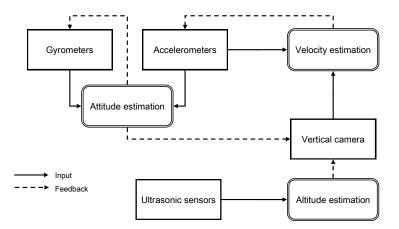














Use of magnetometers

- Problem : perturbations created by the quadrotor, static and dynamic
- Factory calibration to eliminate intrinsic distortion
- Off-line modeling of motor magnetic field function of rotation speed
- Onboard identification of static perturbations : soft iron, hard iron
- Roll-pitch compensation / Complementary filter with gyrometers



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HEADING ESTIMATION

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OUTLINE

Calibration Attitude estimation Velocity estimation Navigation scheme **CONTROL ARCHITECTURE** 3 Remote controller Attitude control Hovering control Pilot control



• iPhone, iPod Touch via WiFi network

- Roll and pitch angles directly controlled by controller inclination
- Vertical speed and yaw rate chosen through the GUI
- Automatic take-off and automatic landing





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Two nested loops

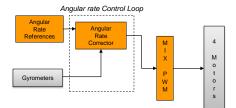
- PI control on angular rate reference
- Angular rate setpoint defined by the attitude setpoint
- Attitude setpoint dependent of the control mode, hovering or flying



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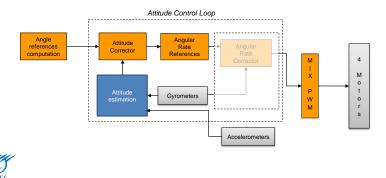
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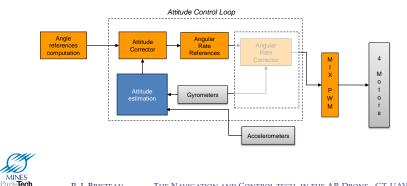


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ParisTech

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- PI control on angular rate reference
- Angular rate setpoint defined by the attitude setpoint
- Attitude setpoint dependent of the control mode, hovering or flying



- In flight mode, setpoint defined by the user
- In hovering mode, setpoint is zero
- Transient given by off-line motion planning with zero speed, zero attitude objectives
 - Inversion of the dynamics

$\dot{u} = -g\theta - C_{\chi}u$

Look-up table from close-loop identification of attitude dynamics, depending of the initial speed.



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 Look-up table from close-loop identification of attitude dynamics, depending of the initial speed

Initial speed	Outdoor hull	Indoor hull
$u_0 < 3 \text{ m.s}^{-1}$	0.7 s	1.5 s
$3 < u_0 < 6 \text{ m.s}^{-1}$	1.0 s	2.2 s
$u_0 > 6 { m m.s^{-1}}$	1.5 s	2.4 s

TABLE: Stop times for different initial speed



Zero attitude setpoint

- Zero speed setpoint
- PI controller on speed estimate to compute attitude reference



- Zero attitude setpoint
- Zero speed setpoint

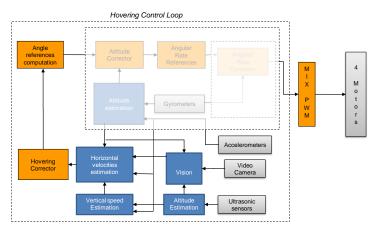
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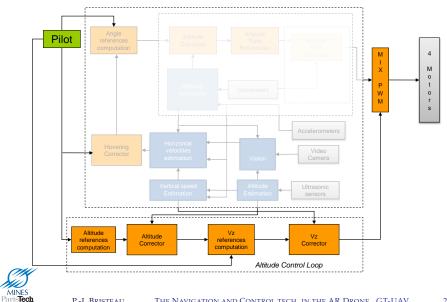


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PILOT CONTROL



P.-J. BRISTEAU

OUTLINE





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- Estimation problem solved without external sensors
 - Complex combination of inertial sensors and vision
 - Exploitation of the different sensors time-horizons
 - Importance of the aerodynamics model.
- Development of low-level control algorithms to guarantee stability and user-friendliness
- Perfect platform to develop guidance and control algorithms



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